

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
7 December 2000 (07.12.2000)

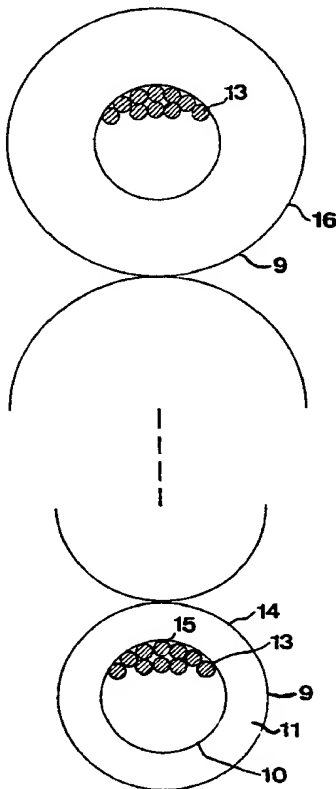
PCT

(10) International Publication Number
WO 00/74212 A1

- (51) International Patent Classification⁷: **H02K 3/40**, 3/42, 3/34, 15/08, H01B 7/30 (74) Agents: **BJERKÉN, Håkan** et al.; Bjerkéns Patentbyrå KB, Box 1274, S-801 37 Gävle (SE).
- (21) International Application Number: PCT/SE00/01059 (81) Designated States (*national*): AE, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CR, CU, CZ, CZ (utility model), DE, DE (utility model), DK, DK (utility model), DM, DZ, EE, ES, FI, FI (utility model), GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SK (utility model), SL, TJ, TM, TR, TT, TZ, UA, UG, US, UZ, VN, YU, ZA, ZW.
- (22) International Filing Date: 25 May 2000 (25.05.2000)
- (25) Filing Language: Swedish
- (26) Publication Language: English
- (30) Priority Data: 9901913-5 27 May 1999 (27.05.1999) SE
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[Continued on next page]

(54) Title: AN ELECTRIC MACHINE WITH LOW EDDY CURRENT LOSSES



(57) Abstract: A rotating electric machine having a magnetic circuit which in one of the parts of a rotor and a stator of the machine comprises an element (1) having a slot for a winding of layers (14, 16) of cables (9) extending substantially axially and arranged substantially radially outside each other, said cables comprising an inner conductor (10) comprising a plurality of strands (13) and an insulation (11) arranged outside thereof, has a larger share of strands of the cables closest to the other part of the rotor and the stator electrically insulated (15) with respect to each other than in the cables in the cable layer (16) most far away from said other part.

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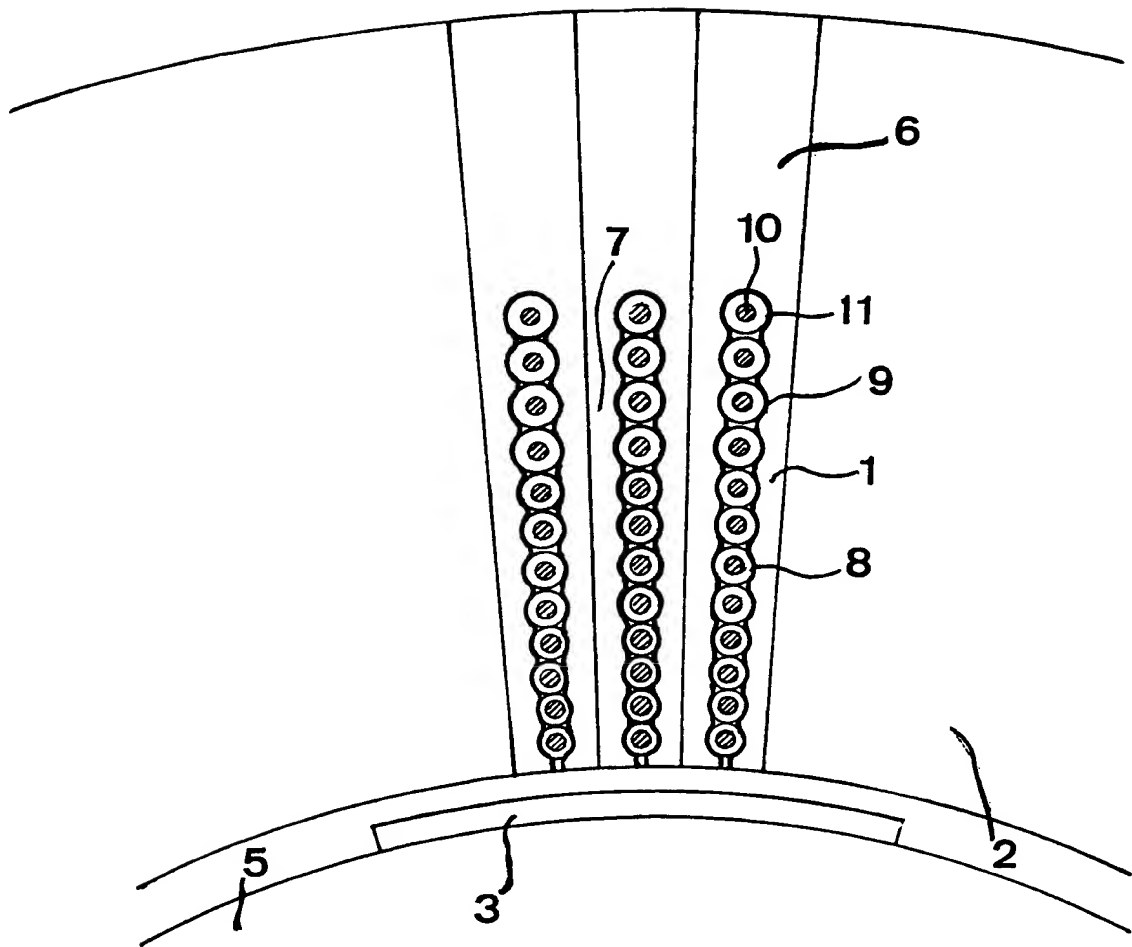
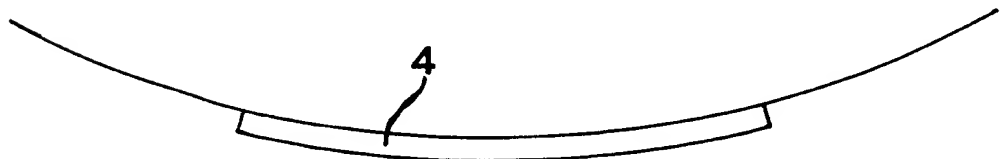
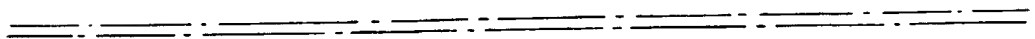


Fig 1



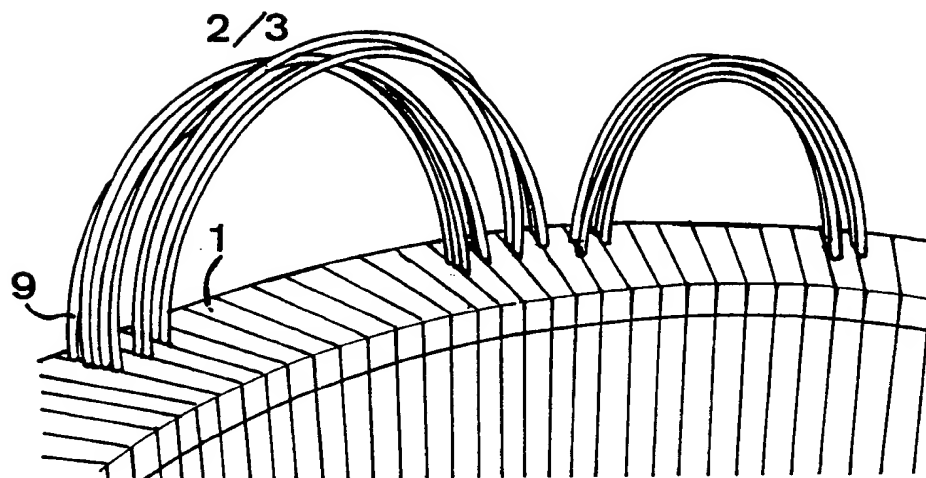


Fig 2

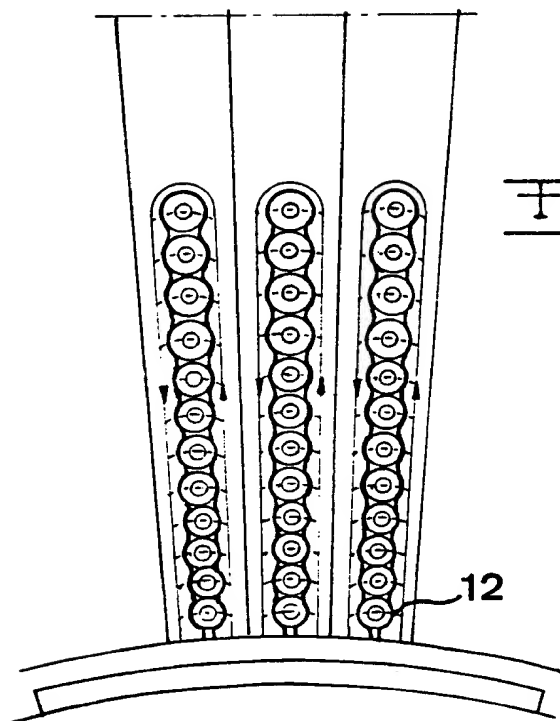


Fig 3

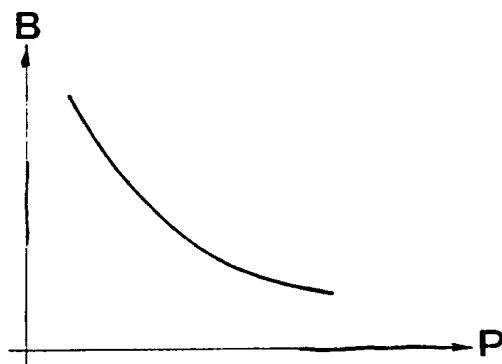
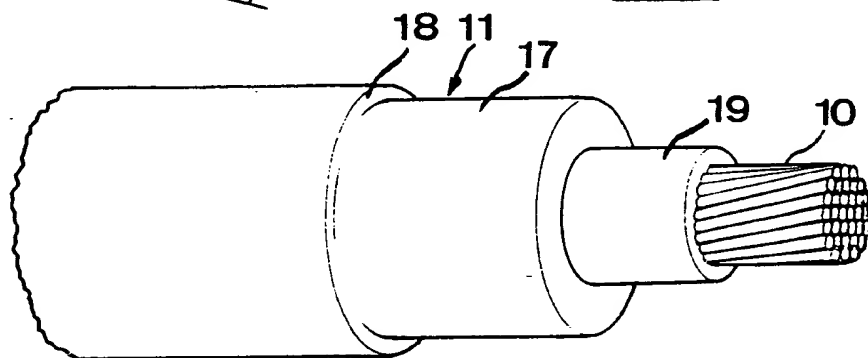


Fig 4

Fig 5



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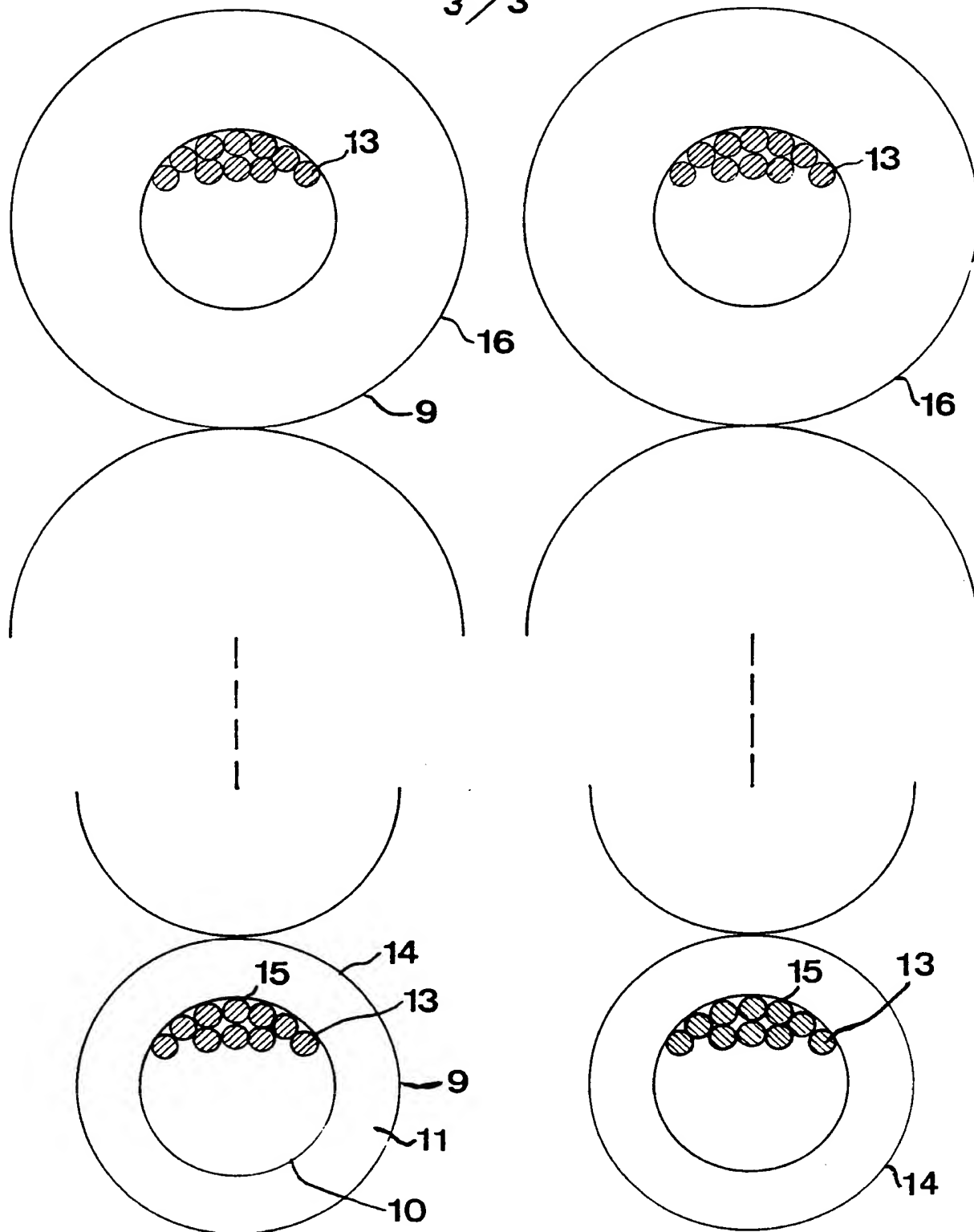


Fig 6

Fig 7



Published:

— With international search report.

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

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AN ELECTRIC MACHINE WITH LOW EDDY CURRENT LOSSES

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FIELD OF THE INVENTION AND PRIOR ART

15 The present invention relates to a rotating electric machine having a magnetic circuit which in one of the parts of a rotor and a stator of the machine comprises an element having a slot for a winding having layers of cables extending substantially axially and arranged substantially radially outside each other, said cables comprising an inner conductor comprising a plurality of
20 strands and an insulation externally thereof.

All types of rotating electric machines of the type with winding of a cable are comprised, i.e. such machines in which there is an insulation sheet around the conductor and the conductor is
25 formed by a bundle of strands. All voltage ranges, high voltage as well as intermediate voltage and low voltage are comprised.

The element in the magnetic circuit with a slot for the cables may as mentioned be arranged in any of the parts: rotor and
30 stator, of the electric machine. "Slot" is here to be given a broad sense and does not necessarily mean that this is so narrow that the element alone keeps the cables in place.

The electric machine may be arranged to function as generator and/or motor. For the purpose of example it may be mentioned
35 that the machine could be a synchronous machine used as gen-

erator for connection to distribution and transmission networks or as motor or for phase compensation and voltage regulation. Other types of machines, such as asynchronous alternating current machines are also conceivable.

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The element has a design allowing an alternating magnet flux therein, and it is preferably but not necessarily formed by a magnetic core of laminated sheet being normal or oriented, i.e. thin sheets being mutually insulated, for example through an insulation lacquer so as to keep the eddy current losses in the
10 element on an acceptable low level.

A rotating electric machine of the type defined in the introduction is for example known through WO 97/45919 of the applicant, and it is schematically illustrated in the appended Fig 1 how an electric machine of that type may be constructed. The
15 element 1 of the magnetic circuit is in this case formed in the stator 2. The rotor with two rotor poles 3, 4 shown (it will in the practice have more, for example four) is designated by 5. The
20 element 1, or actually the stator, is in a conventional way composed by a laminated core of electric sheet successively composed by sector-shaped plates. The number of teeth 7 extends from a back portion 6 of the core located radially outermost radially inwardly towards the rotor. A corresponding number of
25 slots 8 are arranged between the teeth. The slots receive a winding of layers of cables 9 extending substantially axially and arranged radially outside each other. The cables 9 comprise an inner conductor 10 consisting of a plurality of strands and an insulation 11 arranged outside thereof. Since we speak about a
30 high voltage generator and the voltage of the cable layers increases with the distance from the rotor through the connection made here the insulating layers get thicker in the direction away from the rotor. As a consequence of the limited availability of suitable cable dimensions no continuous decrease of the cable
35 insulation towards the rotor has taken place, but cables having

three different dimensions of the cable insulation are used, such as for example for 70 kV, 100 kV and 130 kV.

5 It is illustrated in Fig 3 how the magnetic alternating flux generated in the teeth 7 of the element 1 upon rotation of the rotor extends around the cables arranged in the slot 8 in question. A stray flux will as illustrated by dashed lines 12 be created through the conductors in an attempt of the magnetic flux to make a shortcut. This stray or leak flux involves some inconveniences. Firstly, the main flux is reduced therethrough, which results in a somewhat lower power of the electric machine. Furthermore, the stray flux will generate eddy currents in the strands, which results in heat generation and a demand of cooling the cables, which normally takes place indirectly by cooling the sheet package surrounding them. The strands have been electrically insulated from each other for reducing the eddy current losses, so that the magnetic flux experiences thin surfaces when intersecting the conductors of the cables and thereby the eddy currents and accordingly the eddy current losses will be low. However, this means that the conductors and thereby the cable will be considerably more expensive than if the strands had been uninsulated, and the insulation is usually achieved by painting the strands with an insulating lacquer, which means a load on the environment.

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SUMMARY OF THE INVENTION

The object of the present invention is to provide a rotating electric machine of the type defined in the introduction, in which at least the disadvantage last mentioned of such machines already known has been substantially reduced.

This object is according to the invention obtained by the fact that in such a rotating electric machine a larger share of the strands of the cables closest to the other part of the rotor and the

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stator are electrically insulated with respect to each other than of the cables most far away from the other part.

Thus, the invention utilizes the understanding that the magnitude of the stray or leak flux through the respective cable depends upon the relationship between the flow path closed through the cable and the alternative flow path around the cables, which means that the stray flux decreases for each cable layer in the direction away from the rotor. It has turned out that it is therefore possible to allow considerably larger continuous surfaces in the cable conductors intersected by the magnetic flux farther away from the rotor than closer thereto and thereby larger eddy current loops, since the stray flux is in any way so much lower that the eddy current losses in the conductors are kept on an acceptably low level. By electrically insulate fewer strands with respect to each other in the cables most far away from the other part, in the case discussed above the rotor, than in the cables closer to this other part, considerable costs may be saved. The costs of a strand with an insulation are normally in the order of twice the costs of a strand without insulation. Furthermore, it is when using an insulating lacquer for the insulation in this way possible to spare the environment by a considerably reduced consumption of lacquer when manufacturing the cable. Accordingly, the invention is based on the idea to concentrate on reducing eddy current losses where it is mostly needed, i.e. where the leak or stray flux is the highest.

According to a preferred embodiment of the invention substantially all strands are electrically insulated with respect to each other in the cable layer closest to said other part, which is advantageous, since the leak flux is there the highest and the need to keep the surfaces experienced by this leak flux down on a low level is then also the greatest.

According to another preferred embodiment of the invention substantially none of the strands are electrically insulated with

respect to the rest of the strands in the cable layer located most far away from said other part. Such an advantageous design of the cable in said cable layer is in fact possible, since the leak flux of that cable layer is very low thanks to the short extra way to go for the main flux around the cable layer in the element with a considerably higher magnetic reluctance.

According to another preferred embodiment of the invention the share of strands electrically insulated with respect to the rest of the strands of the cable decreases in the direction away from said other part. The advantages mentioned above of a lack of electric insulation of the strands with respect to each other where it is in fact not needed is hereby obtained. According to other preferred embodiments of the invention said decrease may take place for each cable layer in the direction away from said other part or stepwise after two or more cable layers having the same proportion or share of strands being electrically insulated with respect to each other in the direction away from said other part.

According to another preferred embodiment of the invention the electrical insulation of the strands with respect to each other is obtained by providing the respective insulated strand with an insulating thin envelope surrounding the strand, which according to an embodiment is formed by an insulating lacquer. According to another embodiment the electrical insulation of the strands with respect to each other is obtained by making such electrically insulated strands of aluminium, the surface of which is allowed to oxidate for forming an aluminium oxide layer surrounding the strand. It is in this way possible to do without the insulating lacquer undesirable from the environmental point of view, and aluminium may then advantageously be used for the strands requiring an electrical insulation with respect to each other and for example copper of the strands with no need to be electrically insulated with respect to each other. Thus, the cable or cables most far away from said other part could advanta-

geously have a conductor formed by strands of copper uninsulated with respect to each other, while the cables closest to the other part could have the conductor thereof formed by strands of aluminium. Accordingly, in the case discussed above of a high voltage generator the 70 kV-cables could for example have strands of aluminium, while the 100 kV-cables could have strands of copper.

According to another preferred embodiment of the invention said winding is at least partially formed by a cable in the form of a flexible electric conductor having an envelope able to confine the electric field generated around the conductor. This enables a reduction of electric losses, which in its turn results in a lower temperature of the cable and the surrounding element, which reduces the need of cooling and makes it possible to construct cooling arrangements possibly existing in a more simple way than without such a design of the cable. The cable may be made in the form of a flexible cable, which means substantial advantages with respect to manufacturing and mounting compared to rigid windings prefabricated and traditionally used until today. Furthermore, the use results in an insulation system with an absence of gaseous and liquid insulating material with the disadvantage adhered thereto obtained in this way.

Further advantages as well as advantageous features of the invention appear from the other dependent claims and the following description.

BRIEF DESCRIPTION OF THE DRAWINGS

With reference to the appended drawings, below follows a specific description of preferred embodiments of the invention cited as examples.

In the drawings:

Fig 1 is a simplified axial end view of a rotating electric machine of the type according to the invention,

5 Fig 2 is a perspective view of a part of one end of the stator of the electric machine according to Fig 1 during the manufacturing phase thereof,

10 Fig 3 is a detail view of a part of the machine according to Fig 1 illustrating the magnetic flux paths,

Fig 4 is a graph showing the leak magnetic flux through a cable according to Fig 3 in function of the radial distance of the cable from the rotor,

15 Fig 5 is a view illustrating the construction of a cable particularly suited to be used in a rotating electric machine of the type according to the invention, and

20 Figs 6 and 7 are enlarged detail views of the innermost and the outermost cable layer in a rotating electric machine of the type shown in Fig 1 according to a first and a second preferred embodiment of the invention, respectively.

25 DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS OF THE INVENTION

It is firstly illustrated in Fig 2 how the cables 9 are arranged in the slots in the element 1 by threading them thereinto. All cables are not yet in place here.

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It is illustrated in Fig 4 how the leak flux B decreases for each position P of the cable 9 away from the rotor, i.e. with increasing distance from the rotor. The explanation thereto is that the relationship between the leak flux path and the alternative path for the magnetic flux through the element 1 around the cable layer increases continuously.

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It is illustrated in Fig 6 how this understanding has resulted in a first preferred embodiment of the invention, in which the strands 13 (the entire conductor 10 is of course filled by strands, even if the figures show other things for the sake of simplicity) of the cable layer 14 located closest to the rotor are electrically insulated with respect to each other through a thin insulating layer 15 surrounding each strand, which may be of a conventional insulating lacquer. This is important for keeping the eddy current losses on a low level, since the leak flux is the highest there. However, the strands 13 of the cable layer 16 located most far away from the rotor are not electrically insulated with respect to each other, which is possible since the leak flux there is so low that the eddy current losses are still kept on an acceptably low level. It is by this possible to save financial as well as environmental resources. The strands of the outermost cable may namely be obtained to nearly half the cost with respect to the strands of the innermost cable. It is possible to design the cables between the two extreme cable layers 14, 16, so that the share or proportion of strands electrically insulated with respect to each other decreases for each cable layer or stepwise after two, three or the like subsequent cable layers having the same proportion of insulated strands in the direction away from the rotor. However, it is also possible to have for example all strands electrically insulated with respect to each other for a certain number of cable layers, for example half or two thirds thereof, and then have all strands uninsulated for the rest of the cable layers.

A second preferred embodiment of the invention is illustrated in Fig 7, which differs from the one according to Fig 6 by the fact that the electrical insulation of the strands with respect to each other has been obtained by using aluminium as material for the strands and allowing the surface of the strands to oxidate for forming an aluminium oxide layer 15 surrounding the respective strand. In the case that the strands have not been insulated

copper have been used for the strands, since this is more advantageous through the higher electrical conductivity of copper. Thus, as shown in this Figure, all strands of the innermost cable layer may be of aluminium, while the strands of the outer cable layer 16 are made of copper. The advantage of proceeding in this way for obtaining the electrical insulation of the strands with respect to each other where this is found to be necessary is that the insulating lacquer unpleasant from the environmental point of view does not have to be used. Costs for the strands, especially for the one of copper, are simultaneously saved in the same way as in the embodiment according to Fig 6.

Finally, the construction of a cable of the type particularly well suited to be used in a rotating electric machine of the type according to the invention at high voltages is illustrated in Fig 5, especially in a high voltage generator according to WO 97/45919 discussed further above. This cable has an inner electric conductor 10 with an envelope 11 able to confine the electric field generated around the conductor. This cable has an inner flexible electric conductor 10 and an envelope 11 forming an insulation system, which comprises an insulation 17 formed by a solid insulation material, preferably a material on polymeric basis, and an outer layer 18 having an electrical conductivity being higher than the one of the insulation so that the outer layer through connection to ground or otherwise to a comparatively low potential will be able to on one hand operate to equalize potential and on the other primarily enclose the electric field created as a consequence of said electric conductor 10 interiorly of the outer layer 18. Furthermore, the outer layer should have a resistivity being sufficient for minimizing the electric losses in the outer layer. The insulation system also comprises an inner layer 19, which has said at least one electric conductor 10 arranged interiorly thereof and has an electrical conductivity being lower than the one of the electric conductor but sufficient for making the inner layer to operate for equalizing potential and thereby act equalizing with respect to the electric field outside

the inner layer. Thus, such a cable is of a type corresponding to cables having a solid extruded insulation and today being used within power distribution, for example so called PEX-cables or cables with EPR-insulation. The term "solid insulation material" used means that the winding has to be without any liquid or gaseous insulation, for example in the form of oil. The insulation is instead intended to be formed by a polymeric material. Also the inner and outer layers are formed by a polymeric material, although a semiconducting one. The insulation 18 may be made of a solid thermoplastic material, such as low-density polyethylene (LDPE), high-density polyethylene (HDPE), polypropylene (PP), polybutylene (PB), polymethylpentene (PMP), cross-linked polyethylene (XLPE) or rubber such as ethylene-propylene rubber (EPR) or silicon rubber. With respect to the resistivity of the inner layer and the outer layer this should be within the range $10^{-6}\Omega\text{cm}$ – $100\text{ k}\Omega\text{cm}$, suitably 10^{-3} – $1000\Omega\text{cm}$, preferably 1 – $500\Omega\text{cm}$. The inner and the outer layers have advantageously a resistance which per length meter of the conductor/insulation system is in the range $50\mu\Omega$ – $5\text{ M}\Omega$.

The electric load or stress on the insulation system is reduced as a consequence of the fact that the inner and outer layers of the semiconducting materials around the insulation will tend to form substantially equipotential surfaces and the electric field in the insulation will in this way be distributed comparatively homogeneously over the thickness of the insulation.

The adherence between the insulation material and the inner and outer semiconducting layers has to be uniform over substantially the entire interface thereof, so that no hollow spaces, pores and the like may be created. This is of course particularly important in high voltage applications, and a cable of this type has preferably an insulation system adapted for high voltage, suitably over 10 kV , especially over 36 kV and preferably over $72,5\text{ kV}$. The electrical and thermal stresses occurring at such high voltages make high demands on the insulation material. It

is known that so-called partial discharges, PD, is in general a severe problem for the insulation material in high voltage applications. Should hollow spaces, pores or the like be formed in an insulating layer, inner corona discharges may occur at high electric voltages, whereby the insulation material is gradually degraded and the result could be electrical breakdown through the insulation. This could result in a severe breakdown of the reactor.

It is advantageous that the inner and outer layers and the solid insulation have substantially the same thermal properties for avoiding the generation of such hollow spaces or pores, in which it is particularly important that they have substantially the same coefficient of thermal expansion, so that a perfect adherence between the different layers may be maintained during temperature changes thereof and the cable expands and contracts uniformly as a monolithic body upon temperature changes without any destruction or degradation of the interfaces. The insulation layer is for example a PEX-cable of cross-linked low-density polyethylene and the semiconducting layers of polyethylene with dust and metal particles admixed. Volume changes as a consequence of temperature changes are absorbed entirely as changes of the radius of the cable and thanks to the comparatively small difference of the coefficients of thermal expansion of the layers with respect to the elasticity of these materials, the radial expansion of the cable may take place while avoiding that the layers will get loose from each other.

The cable has also to have a certain flexibility, and it is flexible down to a radius of curvature below 25 times the diameter of the cable so that bending may take place while ensuring a good adherence between the respective layers and the solid insulation. The cable is suitably flexible to a radius of curvature below 15 times the diameter of the cable, and preferably to a radius of curvature below 10 times the diameter of the cable. The E-modulus of the different layers in the insulation system should

be substantially equal so as to not induce any unnecessary shearing stresses in the interfaces between the different layers, so that a reduction of the shearing stresses that may be created between the different layers when exerting the cable to powerful bending resulting in tension stresses on the outside of the bend and compressive stresses on the inside of the bend may take place.

The invention is of course not in any way restricted to the preferred embodiments described above, but many possibilities to modifications thereof will be apparent to a man skilled in the art without departing from the basic idea of the invention as defined in the appended claims.

It would for example be well possible to use other materials than those mentioned above for electrically insulating the strands with respect to each other, and it would also be possible to imagine different combinations of electrical insulation therebetween, so that for example where the leak flux is not that high for example an electrically insulating layer is arranged around a smaller amount of strands, as for example three, for electrically insulating them with respect to another such bundle of strands and obtain a suitable restriction of the size of the surface experienced by the leak flux.

For making the electric machine described further above function at higher voltages it is essential that at least one strand of the cable is in electric contact with the inner semi-insulating layer for forming a equipotential surface, and "substantially all strands are electrically insulated with respect to each other" in the claims is intended to cover this case too.

Claims

1. A rotating electric machine having a magnetic circuit which in one of the parts of a rotor (5) and a stator (2) of the machine comprises an element (1) having a slot (8) for a winding having layers (14, 16) of cables (9) extending substantially axially and arranged substantially radially outside each other, said cables (10) comprising an inner conductor comprising a plurality of strands (13) and an insulation (11) externally thereof, **characterized** in that a larger share of the strands of the cables closest to the other part of the rotor and the stator are electrically insulated with respect to each other than of the cables most far away from the other part.
2. A rotating electric machine according to claim 1, **characterized** in that substantially all strands (13) are electrically insulated with respect to each other in the cable layer (14) closest to said other part.
3. A rotating electric machine according to claim 1 or 2, **characterized** in that substantially none of the strands (13) are electrically insulated with respect to the other strands in the cable layer (16) located most far away from said other part (5).
4. A rotating electric machine according to any of claims 1 to 3, **characterized** in that the share of strands electrically insulated with respect to the rest of the strands (13) of the cable (9) decreases in the direction away from said other part (5).
5. A rotating electric machine according to claim 4, **characterized** in that said decrease takes place for each cable layer in the direction away from said other part (5).
6. A rotating electric machine according to claim 4, **characterized** in that said decrease takes place in steps after two or more cable layers having the same share of strands (13) electrically

insulated with respect to each other in the direction away from said other part (5).

5 7. A rotating electric machine according to any of claims 1-6, **characterized** in that said element (1) having slots (8) is arranged in the stator (2) of the machine.

10 8. A rotating electric machine according to any of claims 1-7, **characterized** in that the magnetic circuit is for high voltage and the potential of the cable layers increases in the direction away from said other part (5), and that the thickness of said insulation (11) of the cables (9) increases continuously or stepwise in the direction away from said other part.

15 9. A rotating electric machine according to any of claims 1-8, **characterized** in that the electrical insulation of the strands (13) with respect to each other is obtained by providing the respective insulated strand with a thin electrically insulating envelope (15) surrounding the strand.

20 10. A rotating electric machine according to claim 9, **characterized** in that the insulating envelope (15) is formed by an insulating lacquer.

25 11. A rotating electric machine according to claim 1-8, **characterized** in that the electrical insulation of the strand (13) with respect to each other is obtained by making such electrically insulated strands of aluminium, the surface of which is allowed to oxidate for forming an aluminium oxide layer surrounding the
30 strand.

35 12. A rotating electric machine according to claim 11, **characterized** in that the electrically uninsulated strands (13) are made of copper and the electrically insulated strands (13) are made of aluminium.

13. A rotating electric machine according to any of claims 1-12, **characterized** in that at least the cable (9) of the layer (14) closest to said other part (5) has all strands (13) made of aluminium and at least the cable of the layer (16) most far away from said other part has all strands (13) made of copper.

14. A rotating electric machine according to any of claims 1-13, **characterized** in that said winding is at least partially formed by a cable (9) in the form of a flexible electric conductor (10) with an envelope (11) able to confine the electric field generated around the conductor.

15. A rotating electric machine according to claim 14, in which the envelope comprises an insulation system, **characterized** in that the insulation system comprises an insulation formed by a solid insulation material (17) and outside thereof an outer layer (18) having an electrical conductivity which is higher than the electrical conductivity of the insulation so that the outer layer may through connection to ground or otherwise comparatively low potential be able to on one hand operate for equalizing potential and on the other substantially enclose the electric field generated as a consequence of said electric conductor (10) inwardly of the outer layer.

16. An electric machine according to claim 14 or 15, in which the envelope comprises an insulation system, **characterized** in that the insulation system comprises an insulation (17) formed by a solid insulation material and an inner layer (19) interiorly thereof, that said at least one electric conductor is arranged interiorly of the inner layer and that the inner layer has an electrical conductivity being lower than the electrical conductivity of the electric conductor but sufficient for making the inner layer to operate to equalize potential and thereby to equalize the electric field outside the inner layer.

17. An electric machine according to claim 15 or 16, **characterized** in that the inner (19) and the outer (18) layers and the solid insulation (17) have substantially equal thermal properties.
- 5 18. An electric machine according to any of claims 15-17, **characterized** in that the inner (19) and/or the outer (18) layer comprise a semiconductor material.
- 10 19. An electric machine according to any of claims 15-18, **characterized** in that the inner layer (19) and/or the outer layer (18) have a resistivity in the range $10^{-6}\Omega\text{cm}$ – $100\text{ k}\Omega\text{cm}$, suitably 10^{-3} – $1000\Omega\text{cm}$, preferably 1 – $500\Omega\text{cm}$.
- 15 20. An electric machine according to any of claims 15-19, **characterized** in that the inner layer (19) and/or the outer layer (18) has a resistance, which per length meter of the conductor/insulation system is in the range $50\mu\Omega$ – $5\text{ M}\Omega$.
- 20 21. An electric machine according to any of claims 15-20, **characterized** in that the solid insulation (17) and the inner layer (19) and/or the outer layer (18) are formed by polymeric material.
- 25 22. An electric machine according to any of claims 15-21, **characterized** in that the inner layer (19) and/or the outer layer (18) and the solid insulation (17) are rigidly connected to each other over substantially the entire interface to ensure adherence also upon flexing and temperature change.
- 30 23. An electric machine according to any of claims 15-22, **characterized** in that the solid insulation and the inner layer (19) and/or the outer layer (18) are formed by materials having a high elasticity to maintain mutual adherence on strains during operation.

24. An electric machine according to claim 23, **characterized** in that the solid insulation (17) and the inner layer (19) and/or the outer layer (18) are of materials having substantially equal E-modulus.

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25. An electric machine according to any of claims 15-24, **characterized** in that the inner layer (19) and/or the outer layer (18) and the solid insulation (17) are formed by materials having substantially equal coefficients of thermal expansion.

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26. An electric machine according to any of claims 15-25, **characterized** in that the inner layer (19) is in electric contact with the at least one electric conductor (10).

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27. An electric machine according to claim 26, **characterized** in that said at least one electric conductor (10) comprises a number of strands (13) and that at least one strand of the electric conductor is at least in part uninsulated and arranged in electric contact with the inner layer.

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28. An electric machine according to any of claims 15-27, **characterized** in that the conductor and its insulation system are designed for high voltage, suitably over 10 kV, in particular over 36 kV and preferably over 72,5 kV.

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29. An electric machine according to any of the preceding claims, **characterized** in that it is adapted to be connected through the windings to a high voltage, suitably over 10 kV, in particular over 36 kV and preferably over 72,5 kV.

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INTERNATIONAL SEARCH REPORT

International application No.
PCT/SE 00/01059

A. CLASSIFICATION OF SUBJECT MATTER

IPC7: H02K 3/40, H02K 3/42, H02K 3/34, H02K 15/08, H01B 7/30
According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC7: H02K, H01B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

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C. DOCUMENTS CONSIDERED TO BE RELEVANT

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X	WO 9745930 A1 (ASEA BROWN BOVERI AB), 4 December 1997 (04.12.97), page 5, line 20 - line 24; page 7, line 24 - page 12, line 18, see whole document; figures --	1-29
A	WO 9745920 A1 (ASEA BROWN BOVERI AB), 4 December 1997 (04.12.97), page 6, line 23 - page 14, line 20 --	1
A	DE 19735748 A1 (SIEMENS AG), 30 July 1998 (30.07.98), abstract --	1

☒ Further documents are listed in the continuation of Box C. ☒ See patent family annex.

* Special categories of cited documents:	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be of particular relevance	"X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
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"O" document referring to an oral disclosure, use, exhibition or other means	
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search 13 Sept 2000	Date of mailing of the international search report 18 -09- 2000
Name and mailing address of the ISA/ Swedish Patent Office Box 5055, S-102 42 STOCKHOLM Facsimile No. +46 8 666 02 86	Authorized officer Hans Bagge af Berga/MN Telephone No. +46 8 782 25 00

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